**IN THE SUBSTITUTE SPECIFICATION:**

Please cancel paragraphs 011, 019, 023 and 024 of the Substitute Specification that was filed with the application. Please replace those cancelled paragraphs with replacement paragraphs, also 011, 019, 023 and 024, as follows.

**[011]** It is of great advantage here that an innermost regulating circuit monitors the temperature of the temperature control medium during its preparation (mixing, heating, cooling) at a very close distance and regulates it, so that an error possibly occurring during processing is detected at the start of the conveying path and is removed by regulation, instead of the error not being detected and steps being taken only ~~taken~~ when it reaches the component.

**[019]** In the above mentioned case, wherein temperature control is not performed <u>by a</u> ~~bya~~ primary circuit 04, but by a heating or cooling unit, the feed-in or the injection point 16 corresponds to the location of the energy exchange by the respective heating or cooling unit, and the actuating member 07, for example, to an output control or the like. The connecting point 10 in the circuit 03 is omitted, since the fluid circulates altogether in the circuit 03, and energy is supplied or removed, or heat or cold is "fed in" at the feed-in point 16. In this case, the heating or cooling unit corresponds to the actuating member 07, for example.

**[023]** Temperature control takes place by a regulating device 21, or a regulating

process 21, which will be described in greater detail in what follows. The regulating device 21, as seen in Fig. 1 is based on a multi-loop, here a triple-loop cascade regulation. An innermost regulating circuit has the sensor S1 shortly downstream of the injection point 16, a first regulator R1 and the actuating member 07, i.e. the valve 07. The regulator R1 is provided with a deviation $\Delta\ \Theta_1$ of the measured value $\Theta_1$ from a corrected command variable $\Theta_{1,soll,k}$, node K1 as the input value and acts, in accordance with its implemented regulation behavior and/or its regulation algorithm, with an actuating order $\Delta$ on the actuating member 07. This means that, depending on the deviation of the measured value $\Theta_1$ from the corrected command variable $\Theta_{1,soll,k}$, it opens or closes the valve 07 or maintains the valve position. The corrected command variable $\Theta_{1,soll,k}$ is now not directly specified by a control device or manually, as is otherwise customary, but is formed with the use of an output value from at least one second, further "outward" located regulating circuit. The second circuit has the sensor S2 located shortly prior to the fluid entry into the component 01, as well as a second regulator R2. The regulator R2 ~~R3~~ is provided with a deviation $\Delta\ \Theta_2$ of the measured value $\Theta_2$ at the sensor S2 from a corrected command variable $\Theta_{2,soll,k}$, node K2, as the input value, and at its output generates a value $d\Theta_1$, output value $d\Theta_1$ in accordance with its implemented regulation behavior and/or its regulation algorithm, which is used for forming the above mentioned corrected command variable $\Theta_{1,soll,k}$ for the first regulator R1. This means that, depending on the deviation of the measured value $\Theta_2$ from the corrected command variable $\Theta_{2,soll,k}$, an influence is brought to bear by the value $d\Theta_l$ on the corrected command variable $\Theta_{1,soll,k}$ of the first regulator R1 to be

formed.

**[024]** In a preferred embodiment of the present invention, the corrected command variable $\Theta_{1,soll,k}$ for the first regulator R1 is formed at a node K1', for example by addition, or subtraction from the value $d\Theta_1$ and a theoretical command variable $\Theta'_{1,soll}$. In turn, the theoretical command variable $\Theta'_{1,soll}$ is formed in a pre- regulation member in regard to the heat flow $V_{WF}$. The pre- regulation member $V_{WF}$, in this case $V_{1,WF}$, subscript 1 for forming the command variable of the first regulating circuit, takes the heat exchange, such as losses etc., of the fluid on a partial path into consideration and is based on empirical values, such as expert ~~asexpert~~ knowledge, calibration measurements, etc.. In this way, the pre-regulation member $V_{1,WF}$ takes the heat or cooling losses along the partial path between the measuring points M1 and M2 into consideration in that it forms an appropriately raised or lowered theoretical command variable $\Theta'_{1,soll}$, which is then processed, together with the value $d\Theta_1$, into the corrected command variable $\Theta_{1,soll,k}$ for the first regulator R1. A connection between the input value, i.e. the command ~~thecommand~~ variable $\Theta_{3,soll}$ or $\Theta'_{2,soll}$ or $\Theta'_{2,soll,n}$, as discussed below, and a corrected output value, such as a modified command variable $\Theta'_{2,soll}$ or $\Theta'_{2,soll,n}$, see below, or $\Theta'_{1,soll,n}$, is fixedly stored in the pre-regulation member $V_{WF}$, which can preferably be changed by parameters, or in another way, as needed.